

# Partial oxidation of methane over rhodium catalysts for power generation applications

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## Abstract

The partial oxidation of methane (POM) to syngas, i.e. H<sub>2</sub> and CO, over supported Rh catalysts was investigated at atmospheric pressure. The influence of support material, Rh loading and the presence of water vapor on the methane conversion efficiency and the product gas composition was studied. The catalysts containing ceria in the support material showed the highest activity and formation of H<sub>2</sub> and CO. By increasing the Rh loading, a decrease of the ignition temperature was obtained. The addition of water vapor to the reactant gas mixture was found to increase the ignition temperature and the formation of hydrogen, which is favorable for combustion applications where the catalytic POM stage is followed by H<sub>2</sub>-stabilized homogeneous combustion.

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## 1. Introduction

Catalytic combustion has been extensively investigated for power generation applications [1,2]. Advantages of this combustion method are low NO<sub>x</sub>, CO and soot emissions, as well as the flexibility to perform the combustion reaction over a wide range of fuel-to-air ratios. Palladium (Pd) has been found to be the most active catalyst for methane combustion under fuel-lean reaction conditions. However, Pd-based catalysts suffer from deactivation at higher temperatures due to the phase transition PdO → Pd<sup>0</sup> and are also strongly inhibited by water [3,4]. An alternative approach is a two-stage process consisting of a catalytic fuel-rich step, where only partial oxidation of the fuel occurs, followed by lean homogeneous combustion. Syngas, i.e. H<sub>2</sub> and CO, is produced under fuel-rich conditions, resulting in a hydrogen-stabilized second stage combustion process. Only limited studies of this combustion concept have been published in the past. Lyubovsky et al. investigated methane combustion under various fuel-to-air ratios for supported Pd, Pt and Rh catalysts demonstrating

benefits such as higher activity during fuel-rich operation [5].

Various metals, such as Rh, Pd, Pt, Ru, Ni, Co and Fe, have been investigated as catalysts for partial oxidation of methane (POM) to syngas (1) [6]. Several studies have reported that especially Rh-based catalysts are suitable for this reaction due to their high activity, syngas selectivity and resistance to carbon deposition [7,8].



This paper deals with an experimental study of the catalytic fuel-rich stage described above, i.e. partial oxidation of methane ( $\lambda = 0.25$ ) to syngas. The influence of support material, Rh loading and the presence of water vapor on the methane conversion efficiency and the product gas composition was studied.

## 2. Experimental

### 2.1. Catalyst preparation

Supported rhodium catalysts were prepared by the incipient wetness impregnation method using Rh(NO<sub>3</sub>)<sub>3</sub>

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as metal precursor. The metal oxides  $\text{ZrO}_2$ ,  $\text{Ce-ZrO}_2$  with 17.5%  $\text{CeO}_2$  (MEL Chemicals) and  $\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$ , all previously calcined at  $500^\circ\text{C}$  for 5 h, were used as support material. The Ce–La mixed oxide was prepared by coprecipitation of the corresponding metal nitrates in ammonia. After noble metal impregnation (0.2–1 wt.%), the catalysts were dried at  $110^\circ\text{C}$  followed by calcination in air at  $800^\circ\text{C}$  for 4 h. Finally, ethanol suspensions of the powders were ball-milled and coated on cordierite monoliths (Corning 400 cpsi, length 10 mm, diameter 14 mm).

## 2.2. Activity tests

Activity tests were conducted in a laboratory-scale quartz glass reactor placed in an electrical furnace. The temperature was monitored by thermocouples inserted before and after the catalyst as well as inside the furnace. The product gas was analyzed for  $\text{CH}_4$ ,  $\text{O}_2$ ,  $\text{CO}_2$ ,  $\text{CO}$  and  $\text{H}_2$ . Nitrogen diluted fuel-rich gas mixtures (3.3%  $\text{CH}_4$ , 1.7%  $\text{O}_2$ ) were introduced to the reactor at a GHSV of  $99,000\text{ h}^{-1}$ . Some tests were performed in the presence of 10% water vapor (GHSV  $110,000\text{ h}^{-1}$ ). Repeated heating and cooling cycles in the temperature range of  $200$ – $750^\circ\text{C}$  were performed for each catalyst whilst measuring the activity.

## 2.3. Catalyst characterization

X-ray powder diffraction (XRD) analysis was carried out on a Siemens D5000 diffractometer scanning  $2\theta$  from  $10$ – $90^\circ$  using monochromatic  $\text{Cu K}\alpha$  radiation. Crystal phases were identified by using JCPDS-files. The BET surface area was measured by  $\text{N}_2$  adsorption/desorption using a Micromeritics ASAP 2010 instrument. The samples were degassed at  $250^\circ\text{C}$  prior to analysis. Temperature programmed reduction (TPR) experiments and oxygen storage capacity (OSC) measurements were performed on selected catalysts using a Micromeritics AutoChem 2910 instrument. The samples (0.5 g) were oxidized in 5%  $\text{O}_2/\text{He}$  at  $700^\circ\text{C}$  for 30 min prior to reduction. After purging the system with Ar, the reduction was carried out in 5%  $\text{H}_2/\text{Ar}$  (30 ml/min) by heating the sample from room temperature to  $800^\circ\text{C}$  at a heating rate of  $10^\circ\text{C}/\text{min}$ . Subsequently, the OSC measurements were conducted by injecting oxygen pulses (1 ml) in a He flow at  $450^\circ\text{C}$  until no more  $\text{O}_2$  uptake could be observed.

## 3. Results and discussion

### 3.1. Catalyst characterization

X-ray diffractograms of the catalysts are presented in Fig. 1. The monoclinic  $\text{ZrO}_2$  phase (peaks at  $28.4$  and  $31.6^\circ$ ) was detected for all zirconia-supported catalysts after calcination at  $800^\circ\text{C}$ . The XRD pattern of the Ce-doped zirconia was characteristic of tetragonal zirconia (peak at  $30.2^\circ$ ). This stabilization of the tetragonal phase by

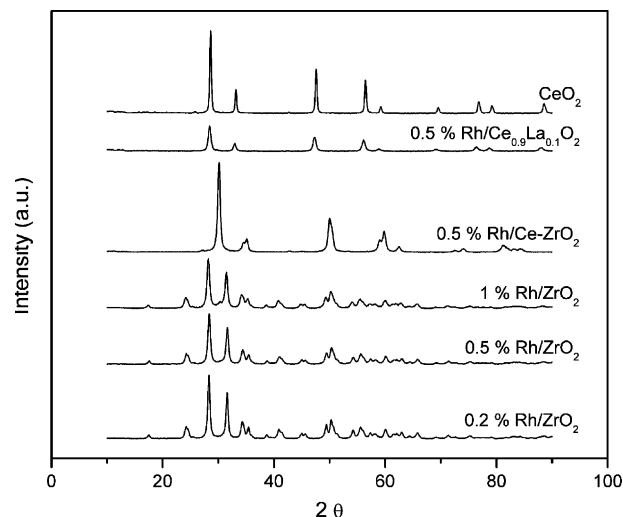


Fig. 1. XRD patterns of Rh catalysts and  $\text{CeO}_2$  after calcination at  $800^\circ\text{C}$  for 4 h.

incorporation of another metal cation has been observed previously [9]. For the mixed oxide containing ceria and lanthana, the XRD data indicated that fluorite-type solid solutions were formed (peaks at  $28.6$  and  $33.1^\circ$ ). The X-ray diffractogram of pure  $\text{CeO}_2$  (peaks at  $28.7$  and  $33.2^\circ$ ), prepared by the same precipitation method, is also displayed in Fig. 1 for comparison. The position of the peaks was shifted to lower  $2\theta$  values when  $\text{La}^{3+}$  ions were integrated in the  $\text{CeO}_2$  crystal lattice due to an increase of the lattice parameter as reported in the past [10]. No segregated phase of lanthanum oxide could be identified. The amount of rhodium in the catalysts was too low to be detected by XRD.

BET surface areas and results from TPR and OSC measurements are listed in Table 1. All catalysts had approximately equal surface areas ( $30$ – $35\text{ m}^2/\text{g}$ ) except for  $0.5\%$   $\text{Rh}/\text{Ce-ZrO}_2$ , which had a slightly higher surface area ( $43\text{ m}^2/\text{g}$ ). The TPR experiments revealed a strong relationship between support material and reduction temperature. The reduction temperature increased in the order of  $\text{Rh}/\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2 < \text{Rh}/\text{Ce-ZrO}_2 < \text{Rh}/\text{ZrO}_2$  for the low-temperature peak, including Rh reduction. A significantly higher intensity of the reduction peaks could be observed for the  $\text{Ce-ZrO}_2$ - and  $\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$ -supported catalysts when compared to  $\text{Rh}/\text{ZrO}_2$  indicating that reduction of the support, as well as of rhodium, occurs at lower temperatures.

Table 1

Textural and redox properties of the catalysts after calcination at  $800^\circ\text{C}$  for 4 h

Sample	BET surface area ( $\text{m}^2/\text{g}$ )	TPR peak temperatures ( $^\circ\text{C}$ )	$\text{O}_2$ uptake ( $\mu\text{mol}/\text{g}$ )	$\text{Ce}^{3+}$ (%)
$0.5\%$ $\text{Rh}/\text{Ce-ZrO}_2$	43	150,585	264	80
$0.5\%$ $\text{Rh}/\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$	35	65,800	321	25
$0.2\%$ $\text{Rh}/\text{ZrO}_2$	29			
$0.5\%$ $\text{Rh}/\text{ZrO}_2$	33	250,530	87	
$1\%$ $\text{Rh}/\text{ZrO}_2$	34			

A very broad and weak reduction peak corresponding to support reduction was also observed in the high-temperature range for all catalysts. Similar results have been reported previously by Fornasiero et al. [11]. According to their study, the addition of rhodium to  $\text{CeO}_2\text{--ZrO}_2$  solid solutions was found to promote low-temperature reduction of the support material due to spill-over of hydrogen from the noble metal to the support.

The OSC measurements revealed a significantly higher  $\text{O}_2$  uptake for  $\text{Ce--ZrO}_2$  and  $\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$  than for  $\text{ZrO}_2$ . The degree of reduction is evaluated from  $\text{O}_2$  uptake measurements and reported as percentage of  $\text{Ce}^{3+}$  in Table 1. Note that noble metal oxidation by  $\text{O}_2$  uptake is not included in the calculations due to the low metal loading. The amount of  $\text{Ce}^{3+}$  was estimated to 80 and 25% for  $\text{Ce--ZrO}_2$  and  $\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$ , respectively. The high oxygen storage capacity of  $\text{CeO}_2$  is related to the ability of the material to shift between reduced and oxidized state, i.e.  $\text{Ce}^{3+}/\text{Ce}^{4+}$  [12]. The addition of dopants, such as Zr and La, to  $\text{CeO}_2$  has been reported to increase the OSC and material stability in several studies [13,14].

### 3.2. Activity tests

The activity tests showed that the rhodium catalysts in this study are active for partial oxidation of methane in the temperature range investigated. The results from the second heating/cooling cycle are always reported in order to obtain a more stable catalytic performance. A slight improvement in activity could be observed during the second heating ramp, probably related to the reduction of  $\text{Rh}_2\text{O}_3$ . An experimental scatter of approximately 5% was thereafter observed. The conversion of methane and oxygen for the catalysts in  $\text{N}_2$ -diluted air is depicted in Fig. 2. Ignition temperatures, defined as the inlet temperature required for 10% conversion of methane, of 300–480 °C were obtained.

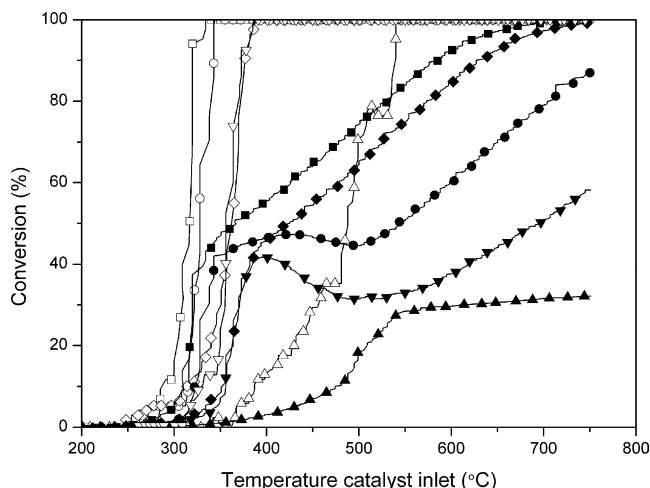


Fig. 2. Conversion of methane (closed symbols) and oxygen (open symbols) in  $\text{N}_2$ -diluted air vs. catalyst inlet temperature for 0.5% Rh/ $\text{Ce--ZrO}_2$  (■), 0.5% Rh/ $\text{Ce}_{0.9}\text{La}_{0.1}\text{O}_2$  (◆), 0.2% Rh/ $\text{ZrO}_2$  (▲), 0.5% Rh/ $\text{ZrO}_2$  (▼) and 1% Rh/ $\text{ZrO}_2$  (●).

Both the support material and the Rh-loading had a significant impact on the catalyst performance. The presence of ceria in the support improved the activity, especially at higher temperatures, and complete conversion could be obtained. This behavior is probably related to the high oxygen mobility of ceria. Previous studies have shown that the addition of Ce to  $\text{ZrO}_2$  increases the activity and stability of Pt and Ni catalysts for partial oxidation of methane due to an increased  $\text{CH}_4$  dissociation and enhanced carbon elimination from the surface [15,16]. Although, carbon deposition should not be a significant problem for the Rh-based catalysts investigated in this work.

The superior activity of the catalysts containing ceria in the support is also explained by the higher rhodium reducibility of these materials compared to zirconia-supported catalysts as revealed by TPR experiments (see Table 1). Metallic rhodium is generally considered to be the active phase of the catalyst. For the  $\text{ZrO}_2$ -supported catalysts with a Rh-loading of 0.5–1 wt.%, a decrease in methane conversion could be observed at about 450 °C after ignition had occurred. The reason for this behavior has not been studied in detail. However, it could be related to mass transport limitations, which would influence the reaction at higher temperatures, resulting in an insufficient supply of oxygen. This would not occur for catalysts containing ceria since oxygen can be supplied from the support.

The rapid depletion of oxygen and initial high production of  $\text{CO}_2$  indicate that complete oxidation of methane occurs initially. Note that the temperature at the catalyst inlet has been recorded and not the actual surface temperature of the catalyst, which obviously is higher due to the strong exothermicity of the complete oxidation reaction. Direct partial oxidation and/or reforming reactions can take place when the oxygen conversion is complete due to the high surface temperature. Increasing the Rh-loading from 0.2 to 1 wt.% significantly affected the  $\text{CH}_4$  conversion resulting in a decrease of the ignition temperature by approximately 160 °C.

The product gas composition obtained for the catalysts is presented in Fig. 3. For power generation applications, the absolute values of the product concentrations after the catalyst are of importance in order to evaluate the stability of the following homogeneous combustion stage. Simultaneous  $\text{H}_2$ , CO and  $\text{CO}_2$  production can be observed. The  $\text{H}_2$  production follows the same behavior as observed for the methane conversion for all catalysts. The formation of  $\text{CO}_2$  occurs mainly at lower temperatures whereas CO is produced at higher temperatures for the tests performed in  $\text{N}_2$ -diluted air.  $\text{H}_2/\text{CO}$  ratios close to 2 were obtained for these catalysts at 750 °C, indicating that partial oxidation is the overall reaction occurring.

The product gas composition is altered when water vapor is added to the reaction mixture as observed in Fig. 3. Higher amounts of  $\text{CO}_2$  are formed in the entire temperature range whereas less CO is formed. Also, at higher temperatures, the formation of  $\text{H}_2$  was enhanced by adding water resulting in

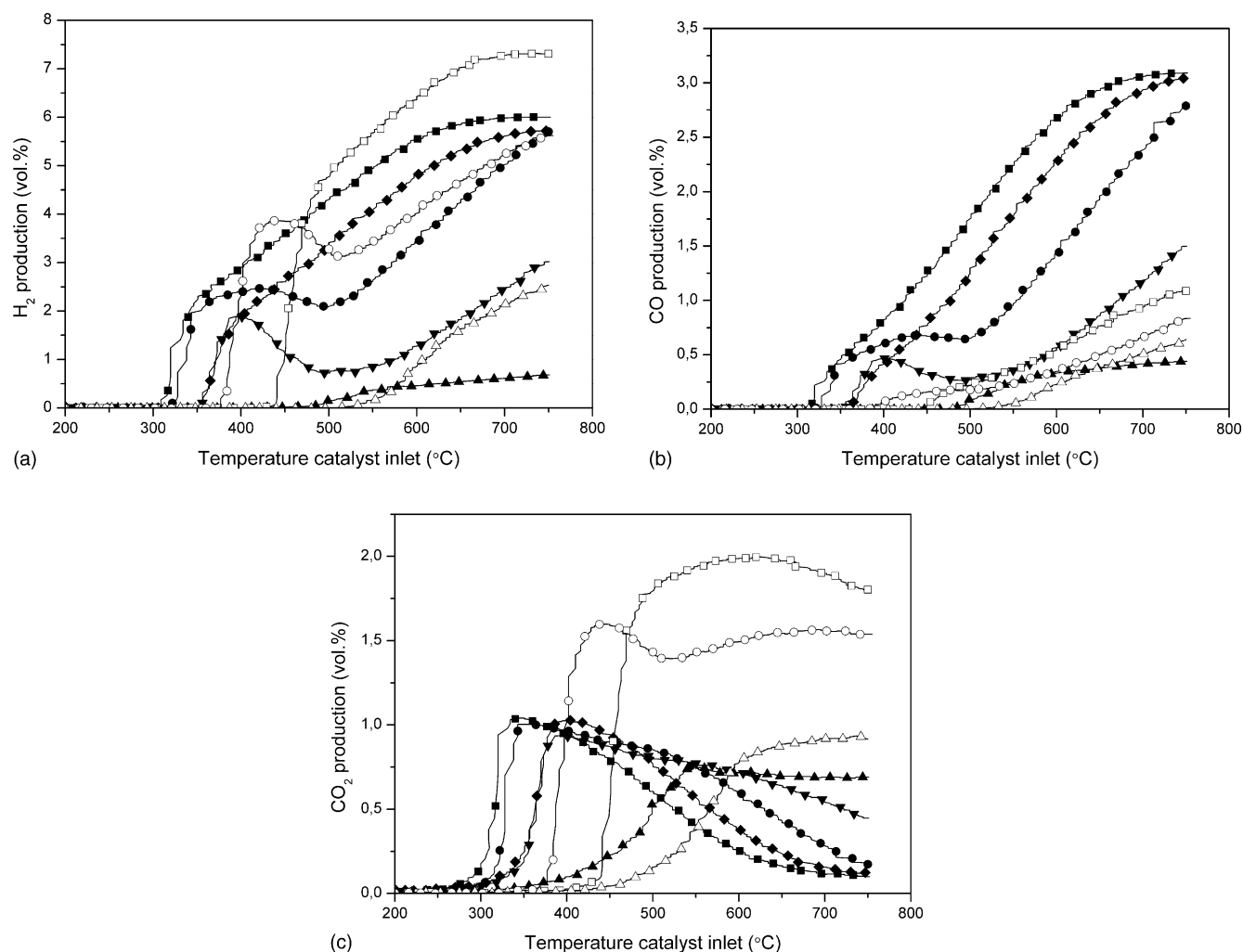


Fig. 3. (a) H<sub>2</sub> production, (b) CO production and (c) CO<sub>2</sub> production in N<sub>2</sub>-diluted air (closed symbols) and in 10% H<sub>2</sub>O/N<sub>2</sub>-air (open symbols) vs. catalyst inlet temperature for 0.5%Rh/Ce-ZrO<sub>2</sub> (■), 0.5% Rh/Ce<sub>0.9</sub>La<sub>0.1</sub>O<sub>2</sub> (◆), 0.2% Rh/ZrO<sub>2</sub> (▲), 0.5% Rh/ZrO<sub>2</sub> (▼) and 1% Rh/ZrO<sub>2</sub> (●).

H<sub>2</sub>/CO ratios higher than 2. Similar trends could be observed for the catalysts not shown in Fig. 3, i.e. 0.5% Rh/Ce<sub>0.9</sub>La<sub>0.1</sub>O<sub>2</sub> and 0.5% Rh/ZrO<sub>2</sub>. The product gas composition is altered due to the water gas shift reaction taking place (2). The high amount of water vapor in the reaction mixture shifts the equilibrium favoring the products H<sub>2</sub> and CO<sub>2</sub>. Furthermore, the addition of ceria was found to increase the catalytic activity.



For the activity tests conducted in the presence of water, the ignition temperature was increased for all catalysts when compared to the experiments performed in N<sub>2</sub>-diluted air (see Fig. 4). The reason for the delay in ignition is presumably due to water adsorbed on the catalyst surface forming hydroxyls, which inhibits the reaction. Additionally, the high-temperature conversion of methane was increased for all ZrO<sub>2</sub>-supported catalysts in the presence of water, which could be due to steam reforming of methane.

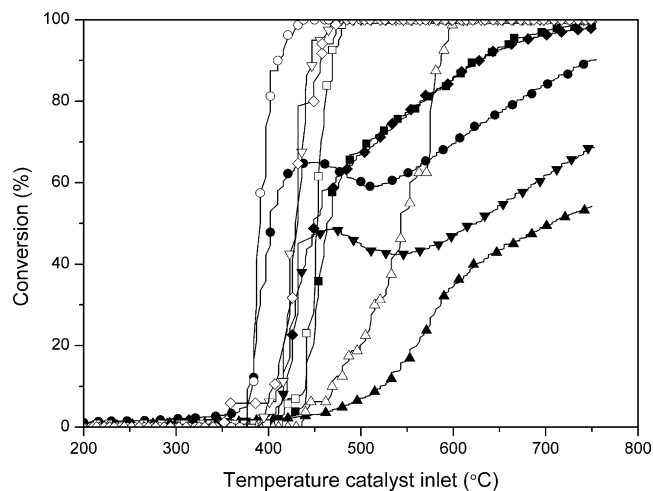


Fig. 4. Conversion of methane (closed symbols) and oxygen (open symbols) in 10% H<sub>2</sub>O/N<sub>2</sub>-air vs. catalyst inlet temperature for 0.5% Rh/Ce-ZrO<sub>2</sub> (■), 0.5% Rh/Ce<sub>0.9</sub>La<sub>0.1</sub>O<sub>2</sub> (◆), 0.2% Rh/ZrO<sub>2</sub> (▲), 0.5% Rh/ZrO<sub>2</sub> (▼) and 1% Rh/ZrO<sub>2</sub> (●).

#### 4. Conclusions

In this study, the investigated Rh-based catalysts were active for partial oxidation of methane. The results from the activity tests revealed a significant importance of the support material on the catalytic behavior. The catalysts containing ceria in the support material showed the highest activity and formation of syngas. The amount of rhodium in the catalyst was also found to influence the behavior significantly. By increasing the Rh loading, a decrease of the ignition temperature was obtained.

The addition of water to the reactant gas mixture increased the ignition temperature for all catalysts. Furthermore, the formation of hydrogen was increased in the presence of water, which is favorable for combustion applications where the catalytic POM stage is followed by H<sub>2</sub>-stabilized homogeneous combustion.

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